

Journal of Applied Research and Technology



www.jart.ccadet.unam.mx Journal of Applied Research and Technology 16 (2018) 276-286

Original

Optimization of friction stud welding process parameters by integrated Grey-Fuzzy logic approach

N. Rajesh Jesudoss Hynes ^a, R. Kumar ^{b,*}, P. Shenbaga Velu ^a, J. Angela Jennifa Sujana ^c

^a Department of Mechanical Engineering, Mepco Schlenk Engineering College, Sivakasi, Tamilnadu, India.

^b Department of Mechanical Engineering, Vels Institute of Science, Technology & Advanced Studies, Pallavaram, Chennai, India.

^c Department of Information Technology, Mepco Schlenk Engineering College, Sivakasi, Tamilnadu, India

Abstract: In this work, an integrated grey fuzzy logic technique is employed for solving the multi-objective function of friction stud welding machine process parameters. This technique converts the multi-objectives into a grey fuzzy reasoning grade. According to the grey fuzzy reasoning grade, an optimal combination of process parameters is concluded. Here, Taguchi L9 orthogonal array is used to design the experiments. The objective of this work is to maximize impact strength and minimize metal loss during the joining of AA 6063 and AISI 1030 steel. Rotational speed, friction time, and friction pressure are considered as the input process parameters. The outcomes of the confirmation test show that good joining strength is accomplished by the optimal level of process parameters.

Keywords: Friction stud welding; aluminum; mild steel; grey-fuzzy logic; impact strength; metal loss

1. INTRODUCTION

Friction stud welding is a solid phase welding performance concerning a stud or appurtenance being rotated at high speed while being forced against a substrate, producing heat by friction (Ates, Turker, & Kurt, 2007). The metal surfaces reach a temperature as a result of which they flow plastically under pressure,

Peer Review under the responsibility of Universidad Nacional Autónoma de México.

The maximum temperatures reached for the duration of welding are much lower than the melting point of the metals. It is a novel variant of the friction welding process. Various factors such as rotational speed, friction time, friction pressure, forging pressure, among others, have an impact on the quality of friction stud welded joints (Mumin, ErolAkata, & Kaan, 2008; Ozdemir, Sarsilmaz, & Hascalik, 2007). Benefits of this welding process are low production time, high reproducibility and low consumption of energy (Fauzi, Uday, Zuhailawati, & Ismail, 2010; Ozdemir, 2005). The friction stud welding

surface impurities are ejected and a forged weld is formed.

^{*} Corresponding author.

E-mail address: mepcokumar@gmail.com (R. Kumar).

process (Hynes, Nagaraj, Palanichamy, Arumugham, & Sujana, 2014) is preferably suited for deep water naval applications, short-term emergency repairs and for submarine rescue. Ocean engineers practiced the application commercially for offshore platform repairs. Additionally, Aluminum/stainless steel friction stud welded joints are necessary for pipes of tanks of liquid propellants in satellite launch vehicles and rocket fuel tanks. In recent times, there is a requisite of joining a steel ear thing pin, which is in the shape of a stud to an aluminum car body.

The main advantage of friction stud welding is the capability to join similar and dissimilar metals (Hong, et al., 2015; Hynes, Nagaraj, & Sujana, 2012).

Usually, welding of dissimilar metals pose some problems as a consequence of the growth of the intermetallic phase during the arc welding methods. For this reason, dissimilar metals cannot be joined using ordinary welding processes (Hynes, Nagaraj, & Sujana, 2014). For the welding of dissimilar metals, friction welding processes have gained importance in the last two decades (Tracie, 2011). The demand for aluminum-low carbon steel and especially aluminum-stainless steel joints has therefore increased in many areas including spacecraft, cryogenic, high vacuum chambers and cooking utensils due to their superior properties (Taban, Gould, & Lippold, 2010). In these structures, aluminum has been partially exchanged by stainless steel and it becomes essential to join stainless steel to aluminum alloys (Fuji, 2004; Reddy, Rao, & Mohandas, 2008; Yokovama, 2003). Aluminum-mild steel friction welding has resulted in considerable cost savings, in the production of down hanger assemblies. In an investigation, the authors reported the joining of aluminum alloy with stainless steel by friction welding (Kong, Chan, & Lee, 2009). In the same way, other researchers carried out experimentation in order to estimate the tensile properties of aluminum-stainless steel friction welded components (Sahin, 2008). The strength and quality of dissimilar joints chiefly depend on the proper selection of process parameters. Optimization of friction welding parameters is to be carried out in order to achieve best results. In the previous year, some of the researchers have optimized the process parameters of friction welding on multi-response characteristics (Paulraj, Aravindan, & Noorul, 2006).

The influence of process parameters in friction welding of carbon steel with AISI 304 and AA 6082 with AISI 304

joints have been proposed by researchers (Paventhan, Lakshminarayanan, Balasubramanian, 2011: Paventhan, Lakshminarayanan, & Balasubramanian, 2012). They considered input process parameters as friction pressure, forging pressure, friction time and forging time. They implemented the response surface methodology (RSM) for optimizing the process parameters to achieve the maximum tensile strength. Likewise, an examination of the process parameters of friction welding of AISI 904L/ Austenitic Stainless Steel has been reported by authors (Karupanan, Mahendra, Paul, & Abdullah, 2014). In that study, they conducted a set of experiments based on Taguchi L18 orthogonal array, in which parameters such as frictional power, burn-off length, upset power and rotational speed were involved. They used grey relational analysis and genetic algorithm to identify the significant factor and optimized level of input parameters in the responses like fatigue life, width and welding time, respectively. Also, other researchers studied the influence of process parameters like friction pressure, upsetting pressure, rotational speed and burn-off length on the responses like tensile strength and hardness during friction welding of UNS S32205 duplex stainless steel (Ajith, Afsal, Sathiya, & Aravindan, 2015). They developed a regression model followed by RSM and optimized the process parameters using the genetic algorithm. Another study of optimization of process parameters of friction welding of AISI 321/ AISI 430 joints using Taguchi L₉ orthogonal array method has been done by authors (Manideep, & Balachandar, 2012).

In that work, they considered process parameters such as friction pressure, upset pressure and burn-off length. They analyzed the metallurgical characteristics and micro hardness across the weld interface. AA6063/AISI 1030 steel joints have many significant applications in the domain of automobile, aerospace and structural applications. The judicial selection of process parameters is based upon the optimal processing conditions achieved through the analysis of the effect of process parameters. In the present work, the objectives are to enhance the joint strength and to reduce the material consumption during the friction stud welding process. However, optimization of process parameters is done by few researchers, multi-objective optimization using grey-fuzzy technique is rarely reported (Ahilan, Kumanan, & Sivakumaran, 2009; Chiang, Liu, & Chou, 2008). Hence, in the present work, with the intention of maximizing the impact strength and minimizing the metal loss process optimization is carried out using the grey-fuzzy technique. Also, analysis of variance (ANOVA) method is employed to predict the influence of each individual process parameters.

2. MATERIALS AND METHODS

In this work, dissimilar metals AA 6063 and AISI 1030 steel are joined by friction stud welding process and the resulting mechanical properties were examined. Taguchi method is employed to separate factors into controllable process variables and uncontrollable process variables. The controllable process variables include rotational friction pressure and friction time. speed, The uncontrollable variables or noise factors include alignment of cylindrical components during friction welding, the surface finish of mating components, cleanliness of weld surfaces, contamination of oxides at the joint interface etc. The manufacturer has no control over these noise factors (Phadke, 1989). The quality of any friction welded components depends on the appropriate selection of the process parameters. Hence, the influence of the process parameters such as friction time, friction pressure and rotational speed on the impact strength and metal loss of the friction welded AA6063/AISI 1030 steel joints was studied in this present work. The friction pressure is the

amount of friction force applied on the contact area of the components during the friction stud welding process. The frictional force is measured by means of load cell fitted in the friction welding machine. The friction pressure is determined by computing the amount of frictional force acting on the contact area during the friction phase of the friction stud welding process. The levels of rotational speed are 800 rpm (A_1) , 1150 rpm (A_2) and 1600 rpm (A_3) , the levels of friction time are $3 \sec (B_1)$, $5 \sec (B_2)$ and 7sec (B₃), and the levels of friction pressure are 300 kPa (C_1) , 400 kPa (C_2) and 500 kPa (C_3) have been selected in this experimentation. Each process parameters of the friction stud welding have three levels and conduct the experiments based on Taguchi L₉ orthogonal array. The experimental outputs of the friction stud welding process are shown in Table 1. Figure 1 shows the process diagram of the friction stud welding. The friction stud welding process is carried out in four stages. In the first phase, the axial load and rotational speed of the mild steel rod were applied and the two rods were brought nearby the joined surfaces. During the second stage, friction heating takes place at the interface of the two rods. In the third phase, the rotational speed was stopped and upsetting under increased pressure occurs simultaneously. In the final phase, the pressure remains constant until the axial pressure is released.

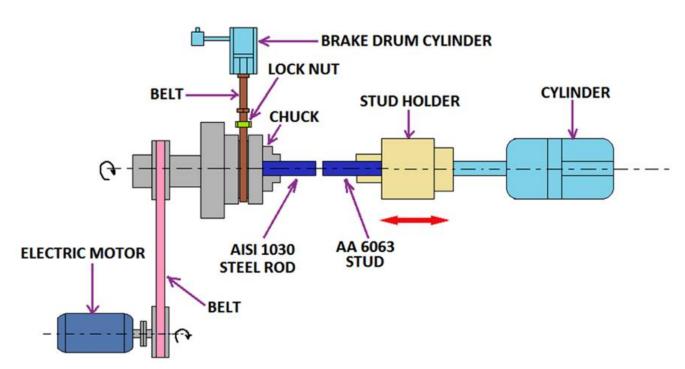


Fig. 1. Schematic diagram of Friction stud welding process.

	Experimental results					Grey fuzzy analysis							
Expt. No	$egin{array}{lll} ext{Rotational} & ext{Friction} \ ext{speed} & ext{time} \ ext{A} & ext{B} \ \end{array}$		time pressure	Impact strength	Metal loss	Normalized data $p_i^*(q)$		$\begin{array}{c} \text{Deviation} \\ \text{sequences} \\ \Delta_{0i}(q) \end{array}$		Grey relational coefficient $\phi_i(q)$		Grey relational grade γι	Grey fuzzy reasoning grade
	rpm	sec kPa	kPa	$ m kJ/m^2$	mm	Impact strength	Metal loss	Impact strength	Metal los	Impact strength	Metal loss	-	λ_0
1	800	3	300	112.50	6.26	0.0000	1.0000	1.0000	0.000	0.3333	1.0000	0.667	0.670
2	800	5	400	125.00	6.46	0.1053	0.9338	0.8947	0.0662	0.3584	0.8830	0.621	0.632
3	800	7	500	137.50	6.6	0.2105	0.8874	0.7895	0.1126	0.3877	0.8162	0.601	0.610
4	1150	3	400	150.00	7.42	0.3158	0.6158	0.6842	0.3841	0.4222	0.5655	0.493	0.500
5	1150	5	500	225.00	7.81	0.9474	0.4868	0.0526	0.5132	0.9048	0.4935	0.699	0.700
6	1150	7	300	231.25	7.59	1.0000	0.5596	0.0000	0.4404	1.0000	0.5317	0.766	0.750
7	1600	3	500	200.00	8.89	0.7368	0.1291	0.2632	0.8709	0.6552	0.3647	0.509	0.516
8	1600	5	300	190.00	8.86	0.6526	0.1391	0.3474	0.8609	0.5901	0.3674	0.479	0.479

Table 1. Experimental and grey-fuzzy analysis results.

3. GREY-FUZZY ANALYSIS

9

1600

The grey-fuzzy analysis combines the two techniques. They are grey relational analysis (GRA) and fuzzy logic (FL). In this analysis, the complicated multi-objective problem is converted into a single-objective problem by means of applying the GRA technique and then uncertainty, such as vagueness or imprecision in the output of GRA technique, is completely reduced by FL technique (Liu, Horng, & Chiang, 2009). In the friction stud welding of AA6063 with AISI 1030 steel metals, the criteria considered necessary to achieve the better quality performance are higher impact strength and lower metal loss.

400

162.50

9.28

0.4211

0.0000

0.5789

1.0000

0.4634

0.3333

0.398

0.400

By using GRA technique, the original sequence data are initially converted into a normalized sequence. Afterwards, the grey relational coefficients (GRC) are calculated for all experimental values. In this work, all welding process parameters influence the responses, therefore equal importance or weight is assigned to those parameters. A higher value of GRC determines the best performance features and the corresponding value will be equal to one. Also, value 1 of GRC represents a maximum

value of the impact strength and a minimum value of the metal loss. Combining FL technique with GRA technique offers an excellent solution to control the uncertainties of imprecision in GRA. Hence, a fuzzy reasoning model is developed for multiple response characteristics and then grey fuzzy reasoning grade is determined for all the experimental values. The steps of the suggested grey-fuzzy logic approach (Gopalakannan, Senthivelan, & Ranganathan, 2013) is used for identifying the optimal level of process parameters of friction stud welding as shown in Figure 2.

Initially, the measured experimental values of impact strength and metal loss are to be converted into normalized sequences of 0 to 1. This step is known as normalization or data preprocessing. In GRA, data preprocessing is required because the difference in the sequence of experimental values are larger. Therefore data preprocessing is needed to diminish the variability of experiment values and converts the original sequence value into a normalized sequence.

Generally, the performance characteristics are categorized into two types. They are larger-the-better (LB) and smaller-the –better (SB). In this work, to achieve the optimal conditions of joint strength, the LB for impact

strength and SB for metal loss are chosen. The performance characteristic normalized value can be determined by the Eq. (1) and (2) respectively,

$$p_i^*(q) = \frac{p_i(q) - \min p_i(q)}{\max p_i(q) - \min p_i(q)}$$
 (1)

$$p_{i}^{*}(q) = \frac{\max p_{i}(q) - p_{i}(q)}{\max p_{i}(q) - \min p_{i}(q)}$$
(2)

where $p_i^*(q)$ represent the normalized sequence after data preprocessing; $p_i(q)$ is the original sequence of S/N ratio value; $\min p_i(q)$ and $\max p_i(q)$ denoted as the smallest value and larger value of $p_i(q)$, respectively; 'q' varies from 1 to 2 and 'i' varies from 1 to 9. If $p_i^*(q)=1$, it denotes as best performance than that of the other alternatives. The calculated normalized values after this data preprocessing step are shown in Table 1. GRC of each output can be calculated by using Eq. (3). It is denoted by the symbol of $\phi_i(q)$ and the results obtained are displayed in Table 1.

$$\phi_{i}(q) = \frac{\Delta_{\min} + \theta \Delta_{\max}}{\Delta_{0i}(q) + \theta \Delta_{\max}}$$
 (3)

The deviation sequence $\Delta_{0i}(\mathbf{q})$ is defined as the absolute difference between the reference sequence and the normalized sequence. The symbols of Δ_{\min} and Δ_{\max} represent the minimum value and maximum value of the deviation sequence, respectively. The distinguishing coefficient is denoted by symbol ϑ and it varies from 0 to 1. In this work, the distinguishing coefficient ϑ is set as 0.5 because this quantity is assigned in most situations. Then the grey relational grade can be determined by averaging the GRC of each performance characteristic. It identifies the degree of effect by the normalized sequence over the reference sequence. It can be denoted in Eq. (4) by symbol (γ_i) .

$$\gamma_i = \frac{1}{i} \sum_{q=1}^i \, \phi_i(\mathbf{q}) \tag{4}$$

Actually, the GRC for each sequence has some degree of uncertainty and vagueness order to define the performance characteristic such as the LB or SB characteristics (Liu et al., 2009). Therefore, based on FL, a fuzzy reasoning of the multi-response characteristics is developed to obtain the optimal processing conditions in a multi-response type problem. The steps which are followed in this fuzzy logic are presented in Figure 3.

In this analysis, three important stages are required to develop the fuzzy reasoning model. They a) fuzzification, which is the formation of membership formation; b)logic rules; and c)defuzzification. The fuzzifier utilizes membership functions (MFs) to fuzzify the GRC initially. A fuzzy inference on the logic rules with the intention of producing a fuzzy value. At last, the defuzzifier utilized to converts the fuzzy value into a grey fuzzy grade. MF defines the fuzziness in a set of fuzzy in which the elements are in the graphical form of discrete or continuous. Mostly used MFs shapes are triangular MFs, trapezoidal MFs, and Gaussian MFs. Fuzzy logic rules are used to create a relationship in between the input and output of fuzzy logic model by way of linguistic statement set. According to the experimental values, construct if then control fuzzy rules, if it is consists of two grey relational coefficients Y_1 , Y_2 and one multi-response output Z which is illustrated as follows:

Rule 1: if Y_1 is P_{11} and Y_2 is P_{21} then Z is Q_1 else Rule 2: if Y_1 is P_{12} and Y_2 is P_{22} then Z is Q_2 else

Rule 9: if Y_1 is P_{19} and Y_2 is P_{29} then Z is Q_9 else.

where P_{1i} , P_{2i} , Q_i are the fuzzy subset of the triangular membership function. The fuzzy multi-response output $\mu Q_0(Z)$ is determined by using max-min interface operation. The fuzzy multi-response output Z can be expressed as follows,

$$\begin{split} \mu Q_0(Z) &= \\ (\mu P_{11}(Y_1) \wedge \mu P_{22}(Y_2) \wedge \mu Q_1(Z)) \wedge \wedge \vee (\mu P_{1i}(Y_1) \wedge \mu P_{2i}(Y_2) \wedge \mu Q_i(Z)) \end{split} \tag{5}$$

The multi-response output of fuzzy is feed into the defuzzifer in order to determine the grey-fuzzy reasoning grade λ_0 in which centroid method is employed. The centroid method expression to find the grey fuzzy reasoning grade is given by the Eq. (6)

$$\lambda_o = \frac{\sum Z\mu Q_0(Z)}{\sum \mu Q_0(Z)} \tag{6}$$

The grey-fuzzy reasoning grade (λ_o) can be able to optimize the complicated multi-responses characteristics. From this grade, a relationship is created in between the factors and which is computed in relation to each response characteristic.

The membership function for impact strength, metal loss, and grey fuzzy reasoning grade are displayed in Figure 4. Here, by using MATLAB R2010a, Mamdani inference engine gets the GRC of impact strength and metal loss as input and generates the grey fuzzy reasoning grade values based on the triangular membership functions along with the rules of fuzzy logic. Three fuzzy subsets were assigned for the grey relational coefficient of impact strength and metal loss and five fuzzy subsets were assigned for grey

fuzzy reasoning grade. GRC of input variables such as impact strength and metal loss is represented by triangular MFs consisting of subsets such as SMALL, MEDIUM and LARGE. In the same way, the output of grey fuzzy reasoning grade is displayed by the MFs as very small (VS), small (S), Medium (M), Larger (L) and very large (VL). Computation of grey fuzzy reasoning grade for all nine experiments is done by the fuzzy logic unit and it is noted in Table 1.

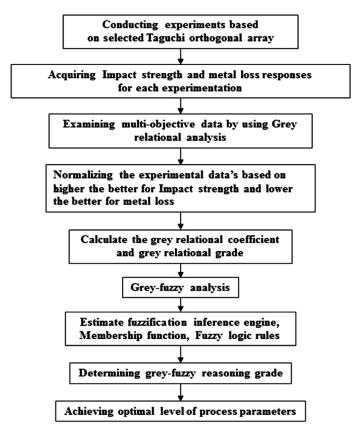


Fig. 2. Procedure of integrated Grey-fuzzy logic analysis.

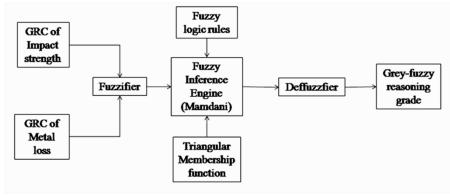


Fig. 3. Structure of the two inputs with one output fuzzy logic.

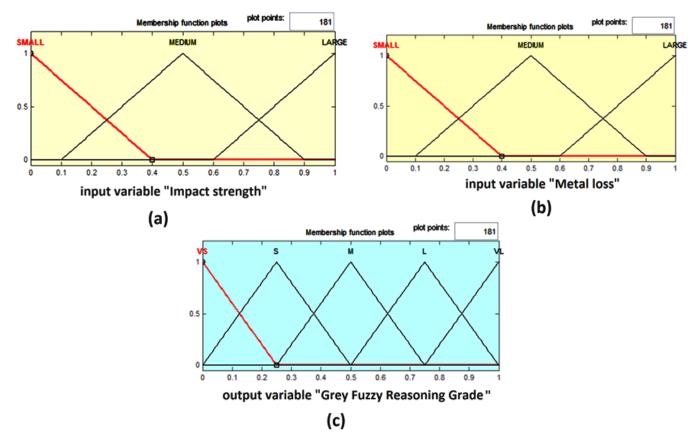


Fig. 4. Membership functions used for this fuzzy logic model.

4. RESULTS AND DISCUSSION

With the intention of finding the optimal level of process parameters of joining accurately, by using grey-fuzzy reasoning grade a response table was established as shown in Table 2. The values in Table 2 denote the average sum of grey-fuzzy reasoning grade for each level of process parameters. Based on maximum grey-fuzzy reasoning grade, an optimal level of process parameter conditions $A_2B_2C_1$ is attained. Optimal process conditions of $A_2B_2C_1$ have larger grey fuzzy reasoning grade values i.e. at the level 2 of rotational speed (0.6500), level 2 of friction time (0.6037) and level 1 of friction pressure (0.6330). Figure 5 shows the effect of grey fuzzy reasoning grade on the rotational speed, friction time and friction pressure.

The grey fuzzy reasoning grades achieved from the experimental values are analyzed by analysis of variance (ANOVA) through a statistical approach. The ANOVA analysis is employed to identify the level of significance of process parameters on the multi objective characteristics of

joining of metals. This analysis is accomplished at a 95 % confidence level.

Fisher's test (F-test) was employed to determine the alternation in which the process parameters of friction stud welding, such as rotational speed, friction time and friction pressure, have a significant influence on the responses like impact strength and metal loss. Larger F-test value demonstrates that the greater influence on the performance characteristics. ANOVA results obtained for the grey-fuzzy reasoning grades are shown in Table 3. This result indicates that rotational speed and friction pressure are the most significant process parameters for affecting the responses such as impact strength and metal loss in friction stud welding joints. The percentage of contribution of rotational speed is 59.36%, friction pressure is 23.30 % and friction time is 2.44 % on multiple responses characteristics such as impact strength and metal loss. After getting the optimal processing conditions (A₂B₂C₁), a confirmation test is necessary to be conducted with the purpose of checking the accuracy of grey-fuzzy analysis and improvement of the multi-responses characteristics. Confirmation results have

been expressed by means of predicted grey fuzzy reasoning grade value $(\check{\lambda})$. By the residual analysis, the prediction of grey fuzzy reasoning grade $(\check{\lambda})$ has been calculated by the following equation (7):

$$\check{\lambda} = \lambda_m + \sum_{i=1}^{N} (\lambda_i - \lambda_m) \tag{7}$$

where λ_m is total mean of grey fuzzy reasoning grade; λ_i is mean of grey fuzzy reasoning grade at an optimal level; N is the number of process parameters that affect the responses characteristics. The predicted grey fuzzy reasoning grade $(\check{\lambda})$ for this work is obtained as 0.7185 and the total mean of grey fuzzy reasoning grade (λ_m) is found to be 0.5841.

Table 4 shows the comparison of the predicted grey-fuzzy reasoning grade value with the actual grey-fuzzy reasoning grade found in the experiment by using the optimal process conditions ($A_2B_2C_1$). It is found that a good correlation is achieved between the predicted value (0.7185) and the experimental value (0.72) of grey-fuzzy reasoning grade. The improvement of grey-fuzzy reasoning grade from the initial parameter conditions ($A_3B_3C_2$) to the optimal parameter conditions ($A_2B_2C_1$) is 0.32. As shown in Table 4, the results of the optimal processing conditions point out that the impact strength value is increased from 162.50 to 220.25 kJ/m², the metal loss is decreased from 9.28 to 7.52 mm.

Symbol	Factors	Grey -	fuzzy reason	Main effect	Rank	
		Level 1	Level 2	Level 3	(max-min)	
A	Rotational Speed (rpm)	0.6373	0.6500^{*}	0.4650	0.1850	1
В	Friction time (sec)	0.5620	0.6037^{*}	0.5867	0.0417	3
C	Friction pressure (kPa)	0.6330^{*}	0.5107	0.6087	0.1223	2

Table 2. Experimental and grey-fuzzy analysis results.

Main Effects Plot for Grey Fuzzy Reasoning Grade

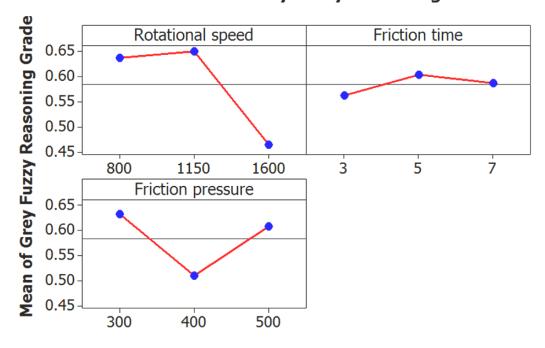


Fig. 5. Effect of grey fuzzy reasoning grade on process parameters.

	Degrees of	Sum of	Mean	F-test value	Percentage of	
Symbol	${\bf freedom}$	square	\mathbf{square}		Contribution	
\mathbf{A}	2	0.064084	0.032042	3.99	59.36	
В	2	0.002634	0.001317	0.16	2.44	
$\overline{\mathbf{C}}$	2	0.025162	0.012581	1.57	23.30	
Residual	2	0.016070	0.008035		14.90	
Error						
Total	8	0.107949			100	

Table 3. Results of the ANOVA for the grey-fuzzy reasoning grade.

Table 4. Result of Confirmation test.

Machining parameters	Initial machining	Optimal machining parameter			
	${f combination}$	Predicted	Experimental		
Setting level	$\mathrm{A_3B_3C_2}$	$A_2B_2C_1$	$A_2B_2C_1$		
Impact strength (kJ/m^2)	162.50	-	220.25		
Metal loss (mm)	9.28	-	7.52		
Grey relational grade	0.400	0.7185	0.72		
Improvement in grey	-	0.3185	0.32		
relational grade					

5. CONCLUSIONS

Joining of dissimilar AA6063/AISI 1030 steel components is attractive to the engineers since it has diverse applications in automotive, aerospace and structural engineering. In the present work, optimal processing conditions are determined using an integrated grey-fuzzy technique to maximizing the impact strength and minimizing the metal loss. The following conclusions have arrived.

- i. Joining of dissimilar metals AA 6063 and AISI 1030 steel with diverse chemical, thermal properties is successfully done using friction stud welding technique. Influence of significant process parameters on the quality and integrity of dissimilar joints are studied.
- ii. Using grey-fuzzy logic technique, maximum impact strength $220.25~\rm kJ/m^2$ and minimum metal loss is $7.52~\rm mm$ is achieved.
- iii. The optimal conditions of friction stud welding process are arrived as rotational speed 1150 rpm, friction time 5 sec and friction pressure 300 kPa.

- iv. ANOVA results indicate that rotational speed, friction pressure and friction time contribute to joint strength by 59.36%, 23.30%, and 2.44% respectively.
- v. The integrated grey-fuzzy logic technique is effectively employed to achieve 26.22% improvement in impact strength and 18.96% reduction in metal loss in AA6063/AISI 1030 steel joints by friction stud welding.

ACKNOWLEDGEMENTS

The authors gratefully acknowledge the financial support for this work by SERB of Department of Science & Technology, New Delhi. (Vide Letter No.: SERB / F / 1452 / 2013-2014 dated 10.06.2013).

CONFLICT OF INTEREST

The authors have no conflicts of interest to declare.

REFERENCES

- Ahilan, C., Kumanan, S., & Sivakumaran, N. (2009). Multi objective optimization of CNC turning process using grey based fuzzy logic, *International Journal of Machining and Machinability of materials*, 5(4), 434-451.
- Ajith, P. M., Afsal, H. T. M., Sathiya, P., & Aravindan, S. (2015). Multi-objective Optimization of Continuous Drive Friction Welding Process Parameters Using Response Surface Methodology with Intelligent Optimization Algorithm. Journal of Iron and Steel Research, 22(10), 954-960
- Ates, H., Turker, M., & Kurt. A. (2007). Effect of friction pressure on the properties of friction welded MA956 iron-based super alloy. *Materials & Design*, 28, 948–953.
- Chiang, K. T., Liu, N. M., & Chou, C. C. (2008). Machining parameter optimization on the die casting process of magnesium alloy using the grey-based fuzzy algorithm, International Journal of Advanced Manufacturing Technology, 38(3-4), 229-237.
- Fauzi, M. N. A., Uday, M. B., Zuhailawati, H., & Ismail, A. B. (2010). Microstructure and mechanical properties of alumina-6061 aluminium alloy joined by friction welding. *Materials & Design*, 31(2), 670-676.
- Fuji, A. (2004). Friction welding of AlMgSi alloy to NiCrMo low alloy steel. Science and Technology of Welding and Joining, 9(1), 83–89.
- Gopalakannan, S., Senthivelan, T., & Ranganathan, S. (2013). Statistical optimization of EDM parameters on machining of aluminium hybrid metal matrix composite by applying taguchi based grey analysis. *Journal of Scientific & Industrial Research*, 72(6), 358-365.
- Hong, M., Guoliang, Q., Peihao, G., Fei, L., Banglong, F., & Xiang, M. M. (2015). Microstructure characterization and properties of carbon steel to stainless steel dissimilar metal joint made by friction welding. *Materials & Design*, 86, 587–597.
- Hynes, N. R. J., Nagaraj, P., Palanichamy, R., Arumugham, C. A. K., & Sujana, J. A. J. (2014). Numerical Simulation of heat flow of Friction Stud Welding of Dissimilar metals. Arabian Journal for Science and Engineering, 39(4), 3217-3224.
- Hynes, N. R. J., Nagaraj, P., & Sujana, J. A. J. (2012). Investigation on Joining of Aluminum and Mild Steel by Friction Stud Welding. *Materials and Manufacturing* Processes, 27(12), 1409-1413.
- Hynes, N. R. J., Nagaraj, P., & Sujana, J. A. J. (2014). Mechanical evaluation and microstructure of friction stud welded aluminium – mild steel joints. Arabian Journal for Science and Engineering, 39(6), 5017-5023.

- Karupanan, B., Mahendra, K. M., Paul, S., & Abdullah, N. S. (2014). Weldability studies and parameter optimization of AISI 904L super austenitic stainless steel using friction welding. *Materials Research*, 17(4), 908-919.
- Kong, T. F., Chan, L. C., & Lee, T. C. (2009). Weld Diffusion Analysis of Forming Bimetallic Components Using Statistical Experimental Methods. *Materials and Manu*facturing Processes, 24(4), 422-430.
- Liu, N. M., Horng, J.T., & Chiang, K. T. (2009). The method of grey-fuzzy logic for optimizing multi-response problems during the manufacturing process: a case study of the light guide plate printing process. *International Journal of Advanced Manufacturing Technology*, 41(1-2), 200-210.
- Manideep, D., & Balachandar, K. (2012). Welding Parameters Metallurgical Properties Correlation of Friction Welding of Austenitic Stainless Steel and Ferritic Stainless Steel, Journal of Applied Sciences, 12(10), 1013-1019.
- Mumin, S., ErolAkata, H., & Kaan, O. (2008). An experimental study on joining of severe plastic deformed aluminium materials with friction welding method. *Materials & Design*, 29(1), 265–274.
- Ozdemir, N. (2005). Investigation of the mechanical properties of friction-welded joints between AISI 304L, AISI Steel as a function rotational speed. *Materials Letters*, 59, 2504–2509.
- Ozdemir, N., Sarsilmaz, F., & Hascalik, A. (2007). Effect of rotational speed on the interface properties of friction-welded AISI 304L to 4340 steel. *Materials & Design*, 28(1), 301–307.
- Paulraj, S., Aravindan, S., & Noorul, H. A. (2006). Optimization for friction welding parameters with multiple performance characteristics. *International Journal of Mechanics and Materials in Design*, 3(4), 309-318.
- Paventhan, R., Lakshminarayanan, P. R., & Balasubramanian, V. (2011). Prediction and optimization of friction welding parameters for joining aluminium alloy and stainless steel. Transactions of Nonferrous Metals Society of China, 21(7), 1480-1485.
- Paventhan, R., Lakshminarayanan, P. R., & Balasubramanian, V. (2012). Optimization of friction welding process parameters for joining carbon steel and stainless steel. *Journal of Iron and Steel Research*, 19(1), 66-71.
- Phadke M.S. (1989) Quality Engineering using Design of Experiments. In: Dehnad K. (eds) Quality Control, Robust Design, and the Taguchi Method, 31-50.
- Reddy, G.M., Rao, A. S., & Mohandas, T. (2008). Role of electroplated interlayer in continuous drive friction welding of AA6061–AISI 304 dissimilar metals. Science and Technology of Welding and Joining, 13(7), 619–628.
- Sahin, M. (2008). Joining of stainless-steel and Aluminium materials by friction welding. The International Journal of Advanced Manufacturing Technology, 4, 487–497.

- Taban, E., Gould, J. E., & Lippold, J. C. (2010). Dissimilar friction welding of 6061-T6 aluminum and AISI 1018 steel: Properties and microstructural characterization. *Materials & Design*, 319 (5), 2305-2311.
- Tracie, P. (2011). Solid-State Joining of Metal Matrix Composites: A Survey of Challenges and Potential
- Solutions. Materials and Manufacturing Processes, 26(4), 636-648.
- Yokoyama, T. (2003). Impact performance of friction welded butt joints between 6061-T6 aluminum alloy and type 304 stainless steel. *Journal of Materials Science & Technology*, 19, 1418-1426.